<span id="page-0-0"></span>

# ±0.8% Accurate Quad UV/OV Positive/Negative Voltage Supervisor

# ADM12914

#### **FEATURES**

**Quad undervoltage/overvoltage (UV/OV) positive/negative supervisor Supervises up to two negative rails Adjustable UV and OV input thresholds Industry leading threshold accuracy over the extended temperature range: ±0.8% 1 V buffered reference output Open-drain UV and OV reset outputs Adjustable reset timeout with disable option Outputs guaranteed down to Vcc of 1 V Glitch immunity 62 μA supply current 16-lead QSOP package Specified from −40°C to +125°C** 

#### **APPLICATIONS**

**Server supply monitoring FPGA/DSP core and I/O voltage monitoring Telecommunications equipment Medical equipment** 

#### **FUNCTIONAL BLOCK DIAGRAM**



#### **GENERAL DESCRIPTION**

The ADM12914 is a quad voltage supervisory IC ideally suited for monitoring multiple rails in a wide range of applications. Each monitored rail has two dedicated input pins, VHx and VLx, which allows each rail to be monitored for both undervoltage (UV) and overvoltage (OV) conditions with high threshold accuracy of  $\pm 0.8$ %. Common active low undervoltage (UV) and overvoltage (OV) pins are shared by each of the monitored voltage rails.

The ADM12914 includes a 1 V buffered reference output, REF, that acts as an offset when monitoring a negative voltage. The three-state SEL pin determines the polarity of the third and fourth inputs, that is, it configures the device to monitor positive or negative supplies.

The device incorporates an internal shunt regulator that enables the device to be used in higher voltage systems. This feature

requires a resistor to be placed between the main supply rail and the  $V_{CC}$  pin to limit the current flow into the  $V_{CC}$  pin at a level no greater than 10 mA. The ADM12914 uses the internal shunt regulator to regulate  $V_{CC}$  if the supply line exceeds the absolute maximum ratings.

The ADM12914 is available in two models. The ADM12914-1 offers a latching overvoltage output that can be cleared by toggling the LATCH input pin. The ADM12914-2 has a disable pin that can override and disable both the  $\overline{\text{UV}}$  and the  $\overline{\text{OV}}$ output signals.

The ADM12914 is available in a 16-lead QSOP package. The device is specified over the extended temperature range of −40°C to +125°C.

#### **Rev. B**

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#### **REVISION HISTORY**



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### <span id="page-2-0"></span>SPECIFICATIONS

T<sub>A</sub> = −40°C to +125°C. Typical values at T<sub>A</sub> = 25°C, unless otherwise noted. V<sub>CC</sub> = 3.3 V, VLx = 0.45 V, VHx = 0.55 V, LATCH = V<sub>CC</sub>,  $SEL = V_{CC}$ ,  $DIS = open$ , unless otherwise noted.

<span id="page-2-1"></span>

<span id="page-2-2"></span> $^{\rm 1}$  The maximum voltage on the V $_{\rm cc}$  pin is limited by the input current. The V $_{\rm cc}$  pin has an internal 6.5 V shunt regulator and, therefore, a low impedance supply exceeding 6 V may exceed the maximum allowable input current. When operating from a higher supply than 6 V, always use a dropper resistor.

## <span id="page-3-0"></span>ABSOLUTE MAXIMUM RATINGS

#### **Table 2.**



Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

#### **Table 3. Thermal Resistance**



#### **ESD CAUTION**



ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

## <span id="page-4-0"></span>PIN CONFIGURATIONS AND FUNCTION DESCRIPTIONS

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8265-002



Figure 2. ADM12914-1 Pin Configuration



Figure 3. ADM12914-2 Pin Configuration

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#### **Table 4. Pin Function Descriptions**

<span id="page-5-0"></span>

<sup>1</sup> N/A means not applicable.

## <span id="page-6-1"></span><span id="page-6-0"></span>TYPICAL PERFORMANCE CHARACTERISTICS



Figure 4. Input Threshold Voltage vs. Temperature





<span id="page-6-2"></span>Figure 6. Vcc Shunt Voltage vs. Temperature



Figure 9. Transient Duration vs. Comparator Overdrive

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### <span id="page-8-0"></span>THEORY OF OPERATION **VOLTAGE SUPERVISION**

The ADM12914 supervises up to four voltage rails for undervoltage and overvoltage conditions. Two pins, VHx and VLx, are assigned to monitor each rail, one for overvoltage detection and the other for undervoltage detection. Each pin is connected to the input of an internal voltage comparator, and its voltage level is internally compared with a 0.5 V voltage reference with very high threshold accuracy of ±0.8%. The device is specified over the extended operating temperature range from −40°C to +125°C.

The output of each of the internal undervoltage comparators is tied to a common UV output pin. Likewise, the outputs of the internal overvoltage comparators are tied to a common  $\overline{\text{OV}}$ output pin.



Figure 16. Typical Applications Diagram

#### **Table 5. Polarity Configuration**

<span id="page-8-1"></span>

#### **POLARITY CONFIGURATION**

The ADM12914 is capable of monitoring supply voltages of both positive and negative polarities. The SEL pin is a threestate pin that determines the polarity of Input 3 and Input 4. As summarized in [Table 5](#page-8-1), the SEL pin is connected to either GND or Vcc, or is not connected.

When an input is configured to monitor a positive voltage, using the three resistor scheme that is shown in [Figure 17](#page-9-1), VHx is connected to the high-side tap of the resistor divider and VLx is connected to the low-side tap of the resistor divider.

Conversely, when an input is configured to monitor a negative voltage, UVx and OVx are swapped internally. The negative voltage for monitoring is then connected as shown in [Figure 18.](#page-9-2) VHx remains connected to the high-side tap and VLx remains connected to the low-side tap. Within this configuration, an undervoltage condition occurs when the monitored voltage is less negative than the programmed threshold, and an overvoltage condition occurs when the monitored voltage is more negative than the programmed threshold.

#### <span id="page-9-0"></span>**MONITORING PIN CONNECTIONS**

#### <span id="page-9-3"></span>**Positive Voltage Monitoring Scheme**

When monitoring a positive supply, the desired nominal operating voltage for monitoring is denoted by  $V_M$ ,  $I_M$  is the nominal current through the resistor divider, V<sub>ov</sub> is the overvoltage trip point, and  $V_{UV}$  is the undervoltage trip point.



Figure 17. Positive Undervoltage/Overvoltage Monitoring Configuration

<span id="page-9-1"></span>[Figure 17](#page-9-1) illustrates the positive voltage monitoring input connection. Three external resistors,  $R_x$ ,  $R_y$ , and  $R_z$ , divide the positive voltage for monitoring,  $V_M$ , into high-side voltage,  $V_{PH}$ , and low-side voltage,  $V_{PL}$ . The high-side voltage is connected to the corresponding VHx pin and the low-side voltage is connected to the corresponding VLx pin.

<span id="page-9-2"></span>To trigger an overvoltage condition, the low-side voltage (in this case, VPL) must exceed the 0.5 V threshold on the VLx pin. The low-side voltage,  $V_{PL}$ , is given by the following equation:

$$
V_{PL} = V_{OV} \left( \frac{R_Z}{R_X + R_Y + R_Z} \right) = 0.5 \text{ V}
$$

Also,

$$
R_X + R_Y + R_Z = \frac{V_M}{I_M}
$$

Therefore,  $R_{Z}$ , which sets the desired trip point for the overvoltage monitor, is calculated using the following equation:

$$
R_Z = \frac{(0.5)(V_M)}{(V_{OV})(I_M)}
$$
 (1)

To trigger the undervoltage condition, the high-side voltage, V<sub>PH</sub>, must exceed the 0.5 V threshold on the VHx pin. The high-side voltage,  $V_{PH}$ , is given by the following equation:

$$
V_{PH} = V_{UV} \left( \frac{R_{Y} + R_{Z}}{R_{X} + R_{Y} + R_{Z}} \right) = 0.5 \text{ V}
$$

Because  $R_z$  is already known,  $R_y$  can be expressed as follows:

$$
R_{Y} = \frac{(0.5)(V_M)}{(V_{UV})(I_M)} - R_Z
$$
 (2)

When  $R_Y$  and  $R_Z$  are known,  $R_X$  is calculated using the following formula:

$$
R_X = \frac{(V_M)}{(I_M)} - R_Z - R_Y \tag{3}
$$

If  $V_M$ ,  $I_M$ ,  $V_{OV}$ , or  $V_{UV}$  change, each step must be recalculated.

#### **Negative Voltage Monitoring Scheme**

[Figure 18](#page-9-2) shows the circuit configuration for negative supply voltage monitoring. To monitor a negative voltage, a 1 V reference voltage is required to connect to the end node of the voltage divider circuit. This reference voltage is generated internally and is output through the REF pin.



Figure 18. Negative Undervoltage/Overvoltage Monitoring Configuration

The equations described previously in the [Positive Voltage](#page-9-3)  [Monitoring Scheme](#page-9-3) section need some minor modifications for use with negative voltage monitoring. The 1 V reference voltage is added to the overall voltage drop; it must therefore be subtracted from  $V_M$ ,  $V_{UV}$ , and  $V_{OV}$  before using each in the previous equations.

To monitor a negative voltage level, the resistor divider circuit divides the voltage differential level between the 1 V reference voltage and the negative supply voltage into high-side voltage,  $V<sub>NH</sub>$ , and low-side voltage,  $V<sub>NL</sub>$ . Similar to the positive voltage monitoring scheme, the high-side voltage,  $V<sub>NH</sub>$ , is connected to the corresponding VHx pin and the low-side voltage,  $V_{NL}$ , is connected to the corresponding VLx pin. Refer to the [Voltage](#page-10-1)  [Monitoring Example](#page-10-1) section for further information.

#### **THRESHOLD ACCURACY**

The reset threshold accuracy is fundamental, especially at lower voltage levels. Consider an FPGA application that requires a 1 V core voltage input with a tolerance of  $\pm 5$ %, where the supply has a specified regulation, for example, ±2.6%. As shown in [Figure 19](#page-10-2), to ensure the supply is within the FPGA input voltage requirement range, its voltage level must be monitored for UV and OV conditions. The voltage swing on the supply itself causes the voltage band available for setting the monitoring threshold to be quite narrow. In this example, the threshold voltages, including the

<span id="page-10-0"></span>tolerances, must fit within a monitor region of just 0.024 V. The ADM12914 device with 0.1% resistors can achieve this level of accuracy.



#### <span id="page-10-2"></span><span id="page-10-1"></span>**VOLTAGE MONITORING EXAMPLE**

To illustrate how the ADM12914 device works in a real-world application, consider the 1 V input example shown in [Figure 19](#page-10-2), with the addition of a −5 V rail.

The first step is to choose the current flow through both voltage divider circuits, for example, 5 μA.

For the 1 V  $\pm$  5% input, due to the specified  $\pm$ 2.6% regulation of the supply, the UV and OV threshold should be set in the middle of the undervoltage and overvoltage monitoring bands, respectively; in this case, on the ±3.8% points of the supply, which are 0.962 V for the UV threshold and 1.038 V for OV threshold.

Input these values into Equation 1 to Equation 3 as follows:

$$
R_Z = \frac{(0.5)(1)}{(1.038)(5 \times 10^{-6})} \approx 96.5 \text{ k}\Omega
$$
 (1)

Insert the value of  $R_z$  into Equation 2.

$$
R_{\gamma} = \frac{(0.5)(1)}{(0.962)(5 \times 10^{-6})} - 96.5 \text{ k}\Omega \approx 7.41 \text{ k}\Omega \tag{2}
$$

Then substitute the calculated values for  $R_z$  and  $R_y$  into Equation 3.

$$
R_X = \frac{1}{5 \times 10^{-6}} - 96.5 \text{ k}\Omega - 7.41 \text{ k}\Omega \approx 96.5 \text{ k}\Omega \tag{3}
$$

This design approach meets the application specifications. As described previously, the 1 V rail is specified with an input requirement of  $\pm 5\%$  and a supply tolerance of  $\pm 2.6\%$ . This effectively means the OV threshold of the monitoring device, including all the tolerance factors, must fit within the 1.026 V to 1.05 V range. Similarly, the UV threshold range must be between 0.95 V and 0.974 V.

The four worst-case scenarios of minimum and maximum undervoltage and overvoltage thresholds are calculated as follows:

Minimum overvoltage threshold

$$
V_{OV\_MIN} = (0.5V - 0.8\%) \left( 1 + \frac{(R_X - 0.1\%) + (R_Y - 0.1\%)}{(R_Z + 0.1\%)} \right)
$$

$$
= 0.496 \left( 1 + \frac{(96,500 + 7410)(0.999)}{(96,500)(1.001)} \right)
$$

$$
= 1.029 \text{ V} > 1.026 \text{ V}
$$

Maximum overvoltage threshold

$$
V_{OV\_MAX} = (0.5 V + 0.8\%) \left( 1 + \frac{(R_X + 0.1\%) + (R_Y + 0.1\%)}{(R_Z - 0.1\%)} \right)
$$
  
= 1.047 V < 1.05 V

The maximum and minimum overvoltage threshold values reside within the 1.026 V to 1.05 V range specified.

The minimum and maximum undervoltage thresholds are calculated as follows:

Minimum undervoltage threshold

$$
V_{UV\_MIN} = (0.5\,\text{V} - 0.8\%) \left( 1 + \frac{(R_X - 0.1\%)}{(R_Y + 0.1\%) + (R_Z + 0.1\%)} \right)
$$

$$
= 0.9557 \; V > 0.95 \; V
$$

Maximum undervoltage threshold

$$
V_{UV\_MAX} = (0.5 \text{ V} + 0.8\%) \left( 1 + \frac{(R_X + 0.1\%)}{(R_Y - 0.1\%) + (R_Z - 0.1\%)} \right)
$$
  
= 0.9729 \text{ V} < 0.974 \text{ V}

These values fit within the specified undervoltage monitoring range. All four worst-case scenarios satisfy the tolerance requirement; therefore, the design approach is valid.



Figure 20. Positive and Negative Supply Monitor Example

Next, consider a -5 V input, which is specified with a ±12% input. The threshold accuracy required by the supply is chosen

<span id="page-11-0"></span>to be within ±5% of the −5 V rail. The UV and OV threshold should be set in the middle of the undervoltage and overvoltage monitoring bands, respectively. In this case, on the  $\pm 8.5\%$ points of the supply, which is −4.575 V for the UV threshold and −5.425 V for the OV threshold.

The negative voltage scheme configuration requires that the 1 V reference voltage be accounted for in Equation 1 to Equation 3. The 1 V reference voltage is subtracted from  $V_M$ ,  $V_{UV}$ , and  $V_{OV}$ , and the absolute value of the result is taken.

Equation 1 becomes

$$
R_Z = \frac{(0.5)(-5-1)}{(-5.425-1)(5 \times 10^{-6})} \approx 93.1 \,\text{k}\Omega
$$

Insert the value of  $R_z$  into Equation 2

$$
R_{Y} = \frac{(0.5)(\left|-5-1\right|)}{(\left|-4.575-1\right)(5\times10^{-6})} - 93.1 \,\text{k}\Omega \approx 14.3 \,\text{k}\Omega
$$

To calculate  $R_x$ , insert the value of  $R_z$  and  $R_y$  into Equation 3.

$$
R_X = \frac{(|-5-1|)}{5 \times 10^{-6}} - (14.3 \text{ k}\Omega) - (93.1 \text{ k}\Omega) \approx 1.09 \text{ M}\Omega
$$

#### **POWER-UP AND POWER-DOWN**

On power-up, when  $V_{CC}$  reaches 1 V, the active low  $\overline{UV}$  output asserts and the  $\overline{\text{OV}}$  output pulls up to V<sub>CC</sub>. When the voltage on the  $V_{CC}$  pin reaches 1 V, the ADM12914 is guaranteed to assert  $\overline{UV}$  low and  $\overline{OV}$  high. When V<sub>CC</sub> exceeds 1.9 V (minimum), the VHx and VLx inputs take control. When  $V_{CC}$  and each of the VHx inputs are valid, an internal timer begins. Subsequent to an adjustable time delay,  $\overline{UV}$  weakly pulls high.

#### **UV/OV TIMING CHARACTERISTICS**

 $\overline{UV}$  is an active low output. It asserts when any of the four monitored voltages is below its associated threshold. When the voltage on the  $V_{CC}$  pin is greater than 2 V, an internal timer holds  $\overline{UV}$  low for an adjustable period, t<sub>voro</sub>, after the voltages on all the monitoring rails rise above their thresholds. This allows time for all monitored power supplies to stabilize after power-up. Similarly, any monitored voltage that falls below its threshold initiates a timer reset, and the internal timer restarts once all the monitoring rails rise above their thresholds.

The  $\overline{UV}$  and  $\overline{OV}$  outputs are held asserted after all faults have cleared for an adjustable timeout period, determined by the value of the external capacitor attached to the TIMER pin.

#### **TIMER CAPACITOR SELECTION**

The  $\overline{\text{UV}}$  and  $\overline{\text{OV}}$  timeout period on the ADM12914 is programmable via the external timer capacitor, CTIMER, placed between the TIMER pin and ground. The timeout period,  $t_{\text{UOTO}}$ , is calculated using the following equation:

 $C_{TIMER} = (t_{UOTO})(115)(10^{-9})$  F/sec

Refer to [Figure 15](#page-7-0) in the [Typical Performance Characteristics](#page-6-1) section, which illustrates the delay time as a function of the timer capacitor value. A minimum capacitor value of 10 pF is required. The chosen timer capacitor must have a leakage current that is less than the 1.7 μA TIMER pin charging current. To bypass the timeout period, connect the TIMER pin to  $V_{CC}$ .



Figure 22. VLx Positive Voltage Monitoring Timing Diagrams

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#### <span id="page-12-0"></span>**UV AND OV RISE AND FALL TIMES**

The  $\overline{UV}$  or  $\overline{OV}$  output rise times (from 10% to 90%) can be approximated using the following equation:

 $t_R \approx 2.2(R_{PULL-UP})(C_{LOAD})$ 

where:

*RPULL-UP* is the internal weak pull-up resistance with an approximate value of 400 kΩ at room temperature with  $V_{CC} > 1$  V. *CLOAD* is the external load capacitance on the output pin.

When a fault occurs, the  $\overline{UV}$  or  $\overline{OV}$  output fall time can be expressed as

 $t_F \approx 2.2(R_{PULL-DOWN})(C_{LOAD})$ 

where  $R_{PULL-DOWN}$  is the internal pull-down resistance, which is approximately 50 Ω. Assuming a load capacitance of 150 pF, the fall time is 16.5 ns.

#### **UV/OV OUTPUT CHARACTERISTICS**

Both the  $\overline{OV}$  and  $\overline{UV}$  outputs have strong pull-down to ground and weak internal pull-up to  $V_{CC}$ . This permits the pins to behave as open-drain outputs. When the rise time on the pin is not critical, the weak pull-up removes the requirement for an external pull-up resistor. The open-drain configuration allows for wire-OR'ing of outputs, which is particularly useful when more than one signal needs to pull down on the output.

At  $V_{\text{CC}} = 1$  V, a maximum  $V_{\text{OL}} = 0.15$  V at  $\overline{\text{UV}}$  is guaranteed. At  $V_{\text{CC}} = 1$  V, the weak pull-up current on  $\overline{\text{OV}}$  is almost turned on. Consequently, if the state and pull-up strength of the  $\overline{OV}$  pin is important at very low  $V_{CC}$ , an external pull-up resistor of no more than 100 kΩ is advised. By adding an external pull-up resistor, the pull-up strength on the  $\overline{\text{OV}}$  pin is greater. Therefore, if it is connected in a wire-OR'ed configuration, the pull-down strength of any single device must account for this additional pull-up strength.

#### **GLITCH IMMUNITY**

The ADM12914 is immune to short transients that may occur on the monitored voltage rails. The device contains internal filtering circuitry that provides immunity to fast transient glitches. [Figure 9](#page-6-2) illustrates glitch immunity performance by showing the maximum transient duration without causing a reset pulse. Glitch immunity makes the ADM12914 suitable for use in noisy environments.

#### **UNDERVOLTAGE LOCKOUT (UVLO)**

The ADM12914 has an undervoltage lockout circuit that monitors the voltage on the  $V_{CC}$  pin. When the voltage on  $V_{CC}$  drops below 1.94 V (minimum), the circuit activates. The UV output is asserted and the  $\overline{\text{OV}}$  output is cleared and is not allowed to assert. When  $V_{CC}$  recovers,  $\overline{UV}$  exhibits the same timing characteristics as though an undervoltage condition had occurred on the inputs.

#### **SHUNT REGULATOR**

The ADM12914 is powered via the  $V_{CC}$  pin. The  $V_{CC}$  pin can be directly connected to a voltage rail of up to 6 V. In this mode, the supply current of the device does not exceed 100 μA. An internal shunt regulator allows the ADM12914 to operate at voltage levels greater than 6V by simply placing a dropper resistor in series between the supply rail and the  $V_{CC}$ pin to limit the input current to less than 10 mA.

Once the supply voltage,  $V_{IN}$ , has been established, an appropriate value for the dropper resistor can be calculated. Begin by determining the maximum supply current required, I<sub>CCtotal</sub>, by adding the current drawn from the reference and/or the pull resistors between the outputs and the  $V_{CC}$  pin to the maximum specified supply current. The minimum and maximum shunt regulator voltage specified in Table 1,  $\rm V_{\rm SHUNT\,min}$  and  $\rm V_{\rm SHUNT\,max}$  are also required in the following calculations.

Calculate the maximum and minimum dropper resistor values

$$
R_{MAX} = \frac{V_{INmin} - V_{SHUNTmax}}{I_{Cctotal}}
$$

$$
R_{MIN} = \frac{V_{INmax} - V_{SHUNTmin}}{100 \,\mu}
$$

Based on these values, choose a real-world resistor value within this range. Then, given the specified accuracy of this resistor, calculate the minimum and maximum real resistor value variation,  $R_{REALmin}$  and  $R_{REALmax}$ , respectively.

The maximum device power is calculated as follows:

$$
P_{DeviceMax} = V_{SHUNTrans} \left[ \frac{(V_{IN max} - V_{SHUNTrans})}{R_{REAL min}} - Icc_{TOTAL} \right] +
$$
  

$$
V_{SHUNTrans} I_{CCtotal}
$$

To check that the calculated value of the resistor will be acceptable, calculate the maximum device temperature rise

$$
Temp_{RISEmax} = \theta_{JA} P_{DeviceMax}
$$

Add this value to the ambient operating temperature. If the resistor value is acceptable, the result will lie within the specified operating temperature range of the device.

#### **OV LATCH (ADM12914-1)**

If an overvoltage condition occurs when the LATCH pin is pulled low, the  $\overline{\text{OV}}$  pin latches low. Pulling LATCH high clears the latch. If an  $\overline{\text{OV}}$  condition clears while  $\overline{\text{LATCH}}$  is high, the latch is bypassed and the  $\overline{\text{OV}}$  pin behaves in the same way as the  $\overline{\text{UV}}$  pin, with an identical timeout period. If the  $\overline{\text{LATCH}}$  pin is pulled low while the timeout period is active, the  $\overline{\rm OV}$  pin latches low, as in normal operation.

#### <span id="page-13-0"></span>**DISABLE (ADM12914-2)**

Pulling the DIS pin high disables both the  $\overline{\rm UV}$  and  $\overline{\rm OV}$  outputs, and forces both outputs to remain weakly pulled high, regardless of any faults that are detected at the inputs. If a UVLO condition is detected, the  $\overline{\text{UV}}$  output is asserted and pulls low;

however, the timeout function is bypassed. As soon as the UVLO condition clears, the  $\overline{\text{UV}}$  output pulls high. To guarantee normal operation when the pin is left unconnected, DIS has a weak 2 μA internal pull-down current.

### <span id="page-14-0"></span>TYPICAL APPLICATIONS



Figure 23. Typical Application Diagram for Monitoring 5 V, 3.3 V, 2.5 V, and 1.8 V with 1.5% Supply Tolerance and 5% Input Tolerance Requirement



Figure 24. Typical Application Diagram for Monitoring 12 V with 1.5% Supply Tolerance and 5% Input Tolerance Requirement; −12 V with 3% Supply Tolerance and 15% Input Tolerance Requirement

### <span id="page-15-0"></span>OUTLINE DIMENSIONS



**CONTROLLING DIMENSIONS ARE IN INCHES; MILLIMETERS DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF INCH EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.**

> Figure 25. 16-Lead Shrink Small Outline Package [QSOP] (RQ-16) Dimensions shown in inches and (millimeters)

#### **ORDERING GUIDE**



1 Z = RoHS Compliant Part.

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